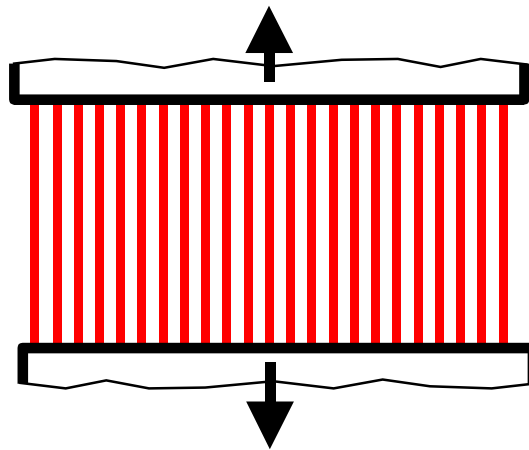




MECHANICS OF PARALLEL FIBER BUNDLES

„TRIVIAL FIBER BUNDLE, TWO-COMPONENT FIBER BUNDLE“



Common variables

for one fiber and
fiber bundle:

h ...gauge length

ε ...strain (relative
elongation)

Other variables and functions:

Number of fibers:

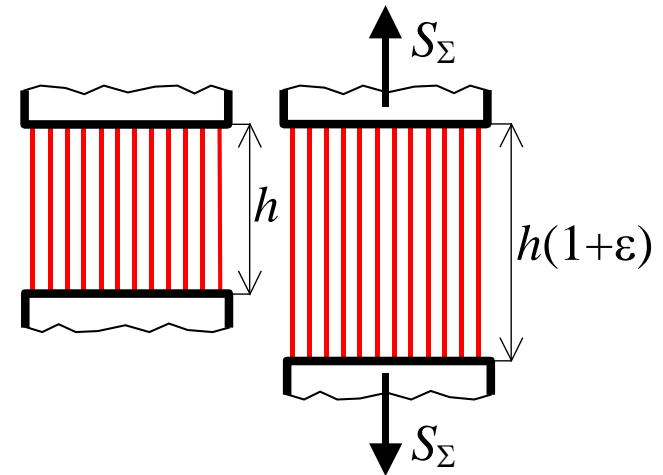
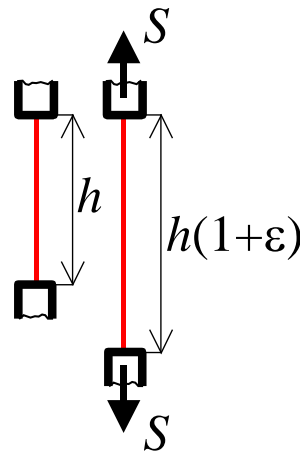
Tensile force:

Force-strain relation:

Strength:

Breaking strain:

One fiber: *Fiber bundle:*



1

n

S

S_{Σ}

$S = S(\varepsilon)$

$S_{\Sigma} = S_{\Sigma}(\varepsilon)$

P (max. of S)

P_{Σ} (max. of S_{Σ})

$a, (P = S(a))$

$a_{\Sigma}, (P_{\Sigma} = S_{\Sigma}(a_{\Sigma}))$

CASE 1 (trivial)

Assumptions: All fibers have

- a) same force-strain curve $S = S(\varepsilon)$ and
- b) same strength P and same breaking strain a .

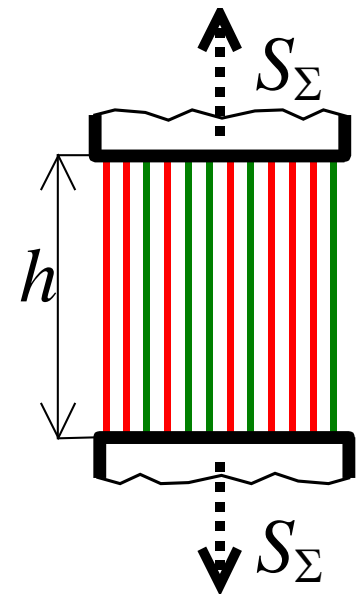
Then the following equations are valid evidently:

$$S_{\Sigma}(\varepsilon) = nS(\varepsilon), \quad P_{\Sigma} = nP, \quad a_{\Sigma} = a$$

CASE 2 (blending theory like W. J. Hamburger)

Assumptions:

1. Fiber bundle is a blend (| and |) of 2 types of fibers.
2. All fibers of one **type have**
 - a) same force-strain curve $S = S(\varepsilon)$ and
 - b) same strength P and same breaking strain a .



Convention:

Fiber of one type having smaller value of breaking strain is denoted as No. 1 (|), other type of fibers is denoted as No. 2. (|). (These numbers are used as subscripts.)

Variables:	Fiber material	
	No. 1	No. 2
Fiber fineness	t_1	t_2
Force-strain relation	$S_1(\varepsilon)$	$S_2(\varepsilon)$
Breaking strain of fiber	$a_1 \leq a_2$	
Fiber strength	$P_1 = S_1(a_1)$	$P_2 = S_2(a_2)$
Number of fibers	n_1	n_2
Total number of fibers	$n = n_1 + n_2$	
Mass of fibers	m_1	m_2
Total mass of fibers	$m = m_1 + m_2$	
Bundle fineness (count)	$T = m/h$	
Mass portion	$g_1 = m_1/m$	$g_2 = m_2/m$
Sum of mass portions	$g_1 + g_2 = 1$	

It is valid for the fiber No. 1:

$$m_1 = g_1 m, \quad t_1 = m_1 / (n_1 h), \quad n_1 = m_1 / (t_1 h) = (g_1 / t_1) \overbrace{(m/h)}^{=T}, \quad n_1 = g_1 (T/t_1)$$

For the fiber No. 2, it is valid analogically:

$$n_2 = g_2 (T/t_2)$$

Maximum forces, in a bundle *Force-strain curves*:

a) Interval $\varepsilon \leq a_1$ max. at $\varepsilon = a_1$

$$S_{\Sigma}(a_1) = n_1 P_1 + n_2 S_2(a_1)$$

$$S_{\Sigma}(a_1) = T \left[g_1 P_1 / t_1 + g_2 S_2(a_1) / t_2 \right]$$

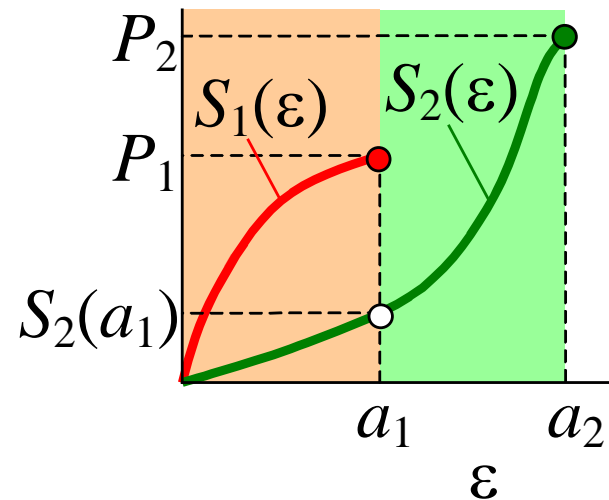
b) Interval $\varepsilon \in (a_1, a_2)$ max. at $\varepsilon = a_2$

$$S_{\Sigma}(a_2) = n_1 \cdot 0 + n_2 P_2$$

$$S_{\Sigma}(a_2) = T g_2 P_2 / t_2$$

c) Interval $\varepsilon > a_2 \Rightarrow$ all fibers are broken,

$$S_{\Sigma}(\varepsilon > a_2) = 0$$



Strength of bundle

$$P_{\Sigma} = \max \{ S_{\Sigma}(a_1), S_{\Sigma}(a_2) \} = T \max \left\{ \left[g_1 \frac{P_1}{t_1} + g_2 \frac{S_2(a_1)}{t_2} \right], \left[g_2 \frac{P_2}{t_2} \right] \right\}$$

P_1/t_1 ...tenacity of fiber No. 1 (e.g. N/tex)

P_2/t_2 ...tenacity of fiber No. 2 (e.g. N/tex)

$S_2(a_1)/t_2$...specific stress of fiber No. 2 (e.g. N/tex) at $\varepsilon = a_1$

Bundle tenacity P_{Σ}/T

$$\frac{P_{\Sigma}}{T} = \max \left\{ \left[g_1 \frac{P_1}{t_1} + g_2 \frac{S_2(a_1)}{t_2} \right], \left[g_2 \frac{P_2}{t_2} \right] \right\} \quad (\text{e.g. N/tex})$$

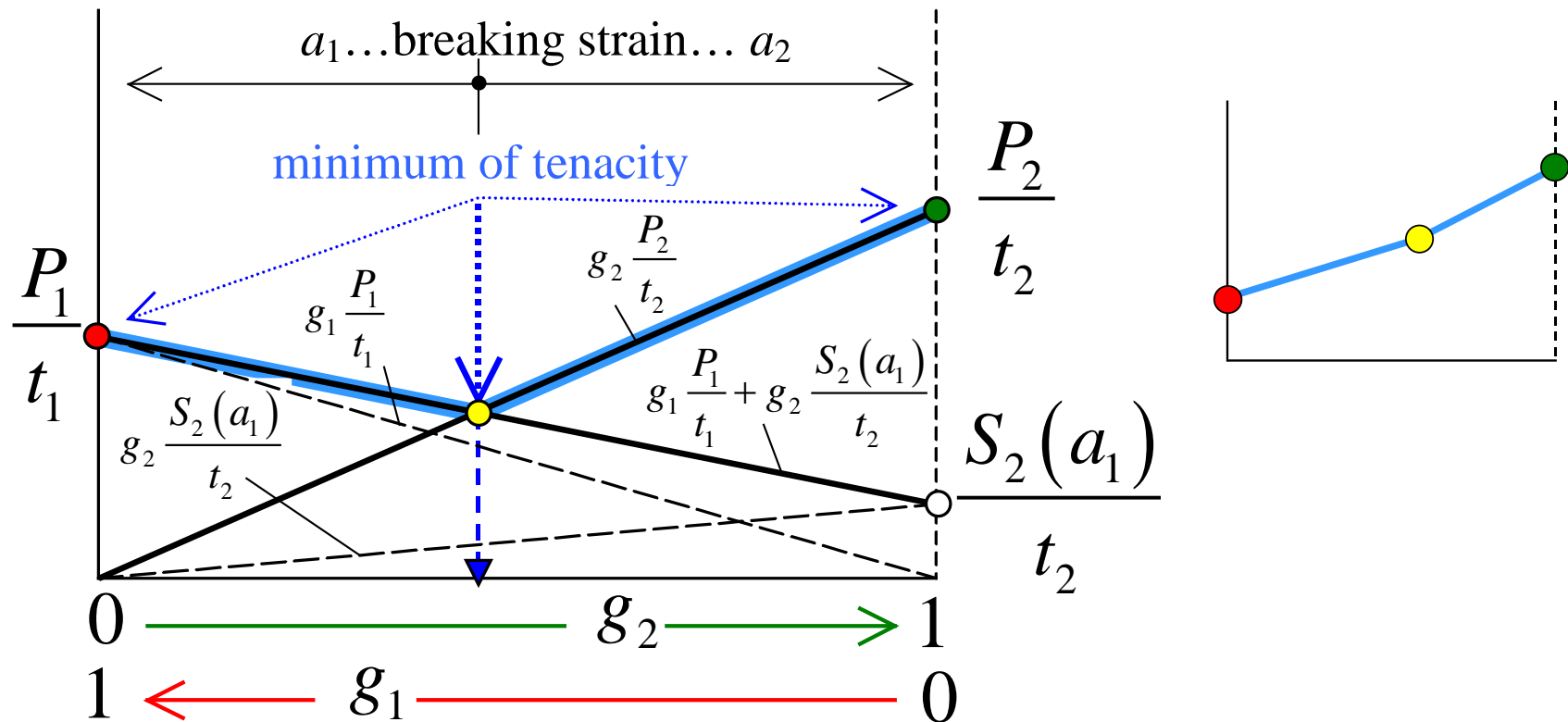
Breaking strain of bundle

a) $a_{\Sigma} = a_1$ if $P_{\Sigma}/T = g_1 P_1/t_1 + g_2 S_2(a_1)/t_2$

b) $a_{\Sigma} = a_2$ if $P_{\Sigma}/T = g_2 P_2/t_2$

Graphical representation of resulting equation

$$P_{\Sigma}/T = \max \left\{ \left[g_1 P_1/t_1 + g_2 S_2(a_1)/t_2 \right], \left[g_2 P_2/t_2 \right] \right\}$$



Minimum bundle tenacity – two possibilities:

a) $g_2 = 0$ (●) and then $P_{\Sigma}/T = P_1/t_1$

b) By point of intersection (●) of two lines, it is

$$\underbrace{=1-g_2}_{g_1} P_1/t_1 + g_2 S_2(a_1)/t_2 = g_2 P_2/t_2,$$

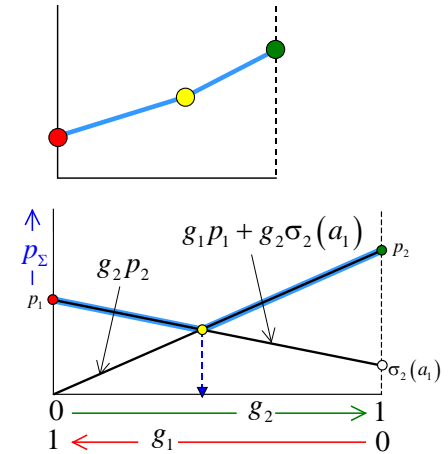
$$P_1/t_1 = g_2 P_1/t_1 + g_2 P_2/t_2 - g_2 S_2(a_1)/t_2,$$

$$g_2 = \frac{P_1/t_1}{P_1/t_1 + P_2/t_2 - S_2(a_1)/t_2}$$

and using of this value we get $P_{\Sigma}/T = g_2 P_2/t_2$

Now, the minimum bundle tenacity is the **minimum of three calculated values** P_{Σ}/T .

Note: After addition of fibers having higher tenacity, the tenacity of resulting bundle can **decrease!**



EMPIRICAL USAGE OF RESULTS FOR YARNS

Instead of fiber parameters, parameters of one component and blended yarns are used.

<i>Quantity</i>	<i>Instead of FIBERS and BUNDLES</i>	<i>we use values of YARNS</i>
ρ_1	Relative strength (tenacity) of fiber with lower breaking strain	Relative strength (tenacity) of one component yarn with lower breaking strain
ρ_2	Relative strength (tenacity) of fiber with higher breaking strain	Relative strength (tenacity) of one component yarn with higher breaking strain
a_1	Breaking strain of fiber of component with lower breaking strain	Breaking strain of one component yarn with lower breaking strain
a_2	Breaking strain of fiber of component with higher breaking strain	Breaking strain of one component yarn with higher breaking strain
$\sigma_{21}(a)$	Relative force in fiber with higher breaking strain by relative elongation $\varepsilon = a_1$	Relative force in one component yarn with higher breaking strain by relative elongation $\varepsilon = a_1$
g_1, g_2	Mass portion of fibers with lower and higher breaking strain in bundle	Mass portion of fibers of one component yarn with lower and higher breaking strain in bundle
ρ_Σ	Relative strength (tenacity) of bundle from two components	Relative strength (tenacity) of blended yarn from two components
a_Σ	Breaking strain of bundle from two components	Breaking strain of blended yarn from two components

Task 1 Calculate number of fibers in bundle, breaking strain of bundle, breaking strength of bundle and relative breaking strength of bundle.

a) 100% cotton, $T=20\text{tex}$, $t=0,17\text{tex}$, $l=26\text{mm}$, $p=0,298\text{Ntex}^{-1}$, $a=9\%$

b) 100% POP, $T=20\text{tex}$, $t=0,188\text{tex}$, $l=40\text{mm}$, $p=0,4\text{Ntex}^{-1}$, $a=63\%$

a) $n=118\text{fibers}$, $a_{\text{bundle}}=9\%$, $P_{\text{bundle}}=5,98\text{N}$, $p_{\text{bundle}}=0,298\text{Ntex}^{-1}$

b) $n=106\text{fibers}$, $a_{\text{bundle}}=63\%$, $P_{\text{bundle}}=7,97\text{N}$, $p_{\text{bundle}}=0,4\text{Ntex}^{-1}$

Task 2 Calculate relative breaking strength of blended yarn
65CO/35POP, yarn count is 20tex, if you know properties of each
component:

100% cotton, $t=0,17\text{tex}$, $p_1=0,183\text{Ntex}^{-1}$, $a_1=6,2\%$

100% POP, $t=0,188\text{tex}$, $p_2=0,231\text{Ntex}^{-1}$, $a_2=24,3\%$

$$\sigma_2(a_1) = a_1 \frac{p_2}{a_2} = 6,2 \frac{0,231}{24,3} = 0,0589 \text{ N/ tex}$$

$$G_2 = \frac{p_1}{p_1 + p_2 - \sigma_2(a_1)} = \frac{0,183}{0,183 + 0,231 - 0,0589} = 0,52$$

$$G_1 = 1 - G_2 = 0,48$$

$$g_2 = 0,35 \Rightarrow p_\Sigma = g_1 p_1 + g_2 \sigma_2(a_1) = 0,65 * 0,183 + 0,35 * 0,0589 = 0,1396 \text{ N/ tex}$$

Task 3 Calculate relative breaking strength of blended yarn
50CO/50PES, yarn count is 25tex, if you know properties of each
component:

100% cotton, $p_1=0,332\text{Ntex}^{-1}$, $a_1=4,9\%$

100% PES, $p_2=0,132\text{Ntex}^{-1}$, $a_2=15\%$

$$\sigma_2(a_1) = a_1 \frac{p_2}{a_2} = 4,9 \frac{0,132}{15} = 0,04312 \text{ N/ tex}$$

$$G_2 = \frac{p_1}{p_1 + p_2 - \sigma_2(a_1)} = \frac{0,332}{0,332 + 0,132 - 0,04312} = 0,79$$

$$G_1 = 1 - G_2 = 0,21$$

$$g_2 = 0,5 \Rightarrow p_\Sigma = g_1 p_1 + g_2 \sigma_2(a_1) = 0,50 * 0,332 + 0,5 * 0,04312 = 0,1876 \text{ N/ tex}$$

Task 4 Calculate relative breaking strength of blended yarn
35CO/65POP, yarn count is 20tex, if you know properties of each
component:

100% cotton, $p_1=0,14\text{Ntex}^{-1}$, $a_1=4,2\%$

100% POP, $p_2=0,42\text{Ntex}^{-1}$, $a_2=9\%$

$$\sigma_2(a_1) = a_1 \frac{p_2}{a_2} = 4,2 \frac{0,42}{9} = 0,196 \text{ N/ tex}$$

$$G_2 = \frac{p_1}{p_1 + p_2 - \sigma_2(a_1)} = \frac{0,14}{0,14 + 0,42 - 0,196} = 0,38$$

$$G_1 = 1 - G_2 = 0,62$$

$$g_2 = 0,65 \Rightarrow p_2 = g_2 p_2 = 0,65 * 0,42 = 0,273 \text{ N/ tex}$$