

## 4. Sensorial comfort of fabrics

### 4.1 Subjective evaluation of fabric handle

Subjective assessment treats fabric hand as a psychological reaction obtained from the sense of touch (Bakar, 2004). Traditionally, in the textile and clothing industries, the assessment of the fabric handle is carried out subjectively by individual judges. The judgements strongly rely on personnel criteria (Yick et al., 1995).

When a person runs their finger across the surface of a fabric, a complex multi-sensory, emotional and cognitive experience takes place. A memory is stirred, an emotion, feeling and association is evoked and a decision is made, an impression becomes embossed in the mind. Decisions and motivations are based on anticipated reality of preference, personality, emotion and moods, for audience or non-audience participation (Moody et al., 2001).

The subjective hand is the result of touch sensation and therefore is dependent on the mechanisms of human tactile sensations. The somatic senses are those nervous system mechanisms by which sensory information is collected from within body. The somatic senses are classified to the three groups:

1. Mechanoreceptors - stimulated by mechanical displacement of various tissues at the body
2. Thermo receptors - stimulated by temperature changes
3. Nocio receptors - representing the human pain sense

It is then clear that subjective hand sensing is the combination of various receptors responsible for feeling of texture, pressure, stretching, thermal feedback, dynamic deformation and vibration and from the sum of their complex responses humans can perceive and discriminate between the textiles (Militky& Bajzík, 1997).

In the subjective assessment process of textiles, fabric hand is understood as a result of psychological reaction through the sense of touch. There are variations in how individuals actually feel textiles because people do not have the same sensory perception of identical occurrences. Affecting aspects can be grouped in sociological factors and the physiological factors.

The other main factors affecting the subjective handle evaluation can be defined as; the judges, the criteria of judgement, assessment conditions, assessment technique, the method of ranking and scaling the assessment, analysis of the results (Mahar et al., 1990; as cited in Brand, 1964; Bishop, 1996). Gender, age, education and cultural backgrounds are potential influencing factors. Female individuals in general respond more delicately and sensitively than male individuals and therefore have a finer assessment of a specific parameter (Mäkinen et al., 2005; as cited in Kweon et al., 2004; as cited in Dillon et al., 2000).

Since the services of expert judges are not widely available for research activities, generally students, laboratory assistants and other consumer groups work as panelists. Such panels should be capable of making consistent judgements of textile attributes and due to the high variability of these panelists compared to the expert judges, larger panel sizes should be preferred, at around 25-30 persons (Bishop, 1996).

In order to ensure the reliability of subjective assessments, it is critical to choose the right expressions for the description of a fabric handle parameter (Mäkinen et al., 2005). There are different sensory attributes identified by numerous authors. These are grouped as given in Table 1 (Hu, 2008). The words "thickness," "thinness," "softness," "stiffness," "slippery," "roughness," "tightness," "fullness" and "pliable" are mostly used expressions to describe the feel of a fabric (Sülar & Okur, 2007).

Generally, in order to evaluate the handle of the fabric, fingers are slid on the surface of the fabric, compressed between the thumb and sign finger. The fingers containing more than

250 sensors per cm<sup>2</sup> are the crucial important organs determining the fabric quality (Bensaid et al., 2006). Tightening of the fabric between fingers gives idea about thickness, bulkiness, compressibility, thermal absorptivity and surface properties of the fabrics, whereas slipping of the fingers on the surface of the fabrics with a pressure renders about structure and elongation of the fabrics (Aliouche & Viallier, 2000).

Stiffness/crispness/pliability/flexibility/limpness	Anti-drape/spread/fullness
Softness/harshness/hardness	Tensile deformation/ bending/surface friction/sheer
Thickness/bulkiness/sheerness/thinness	Compressibility
Weight/heaviness/lightness	Snugness/loosenes
Warmth/coolness/coldness (thermal characteristics)	Clinginess/flowing
Dampness/dryness/wetness/clamminess	Quietness/noisiness
Prickliness/scratchiness/roughness/coarseness/itchiness/tickliness/stickiness/	Smoothness/fineness/silkiness
Looseness/tightness	

Table 1. Sensory attributes of fabrics

There are generally four handle methods for the evaluation of fabric handle, as shown in Figure 6. The multiple finger pinch and the touch-stroke are the most relevant ones.

However, using just the index finger has also proved acceptable. Evaluated properties of the fabrics by these handle techniques are given in Table 2 (Moody et al., 2001; as cited in Dillon & Moody, 2000).



Fig. 6. Handle techniques (1. Touch stroke, 2. Rotating cupped, 3. Multiple finger, 4. Two handed rotation) (Moody et al., 2001)

	Handle Technique	Properties Evaluated
1	Touch-stroke	Surface quality (texture), temperature
2	Rotating cupped action	Stiffness, weight, temperature, comfort, overall texture, creasing
3	Multiple finger pinch: Rotating between the fingers action with one hand (thumb and 1 or 2 fingers)	Texture, stiffness, temperature, fabric structure, both sides of a fabric, friction, stretch (force-feedback)
4	Two handed rotation action	Stretch, sheerness

Table 2. Properties evaluated by different handle techniques (Moody et al., 2001)

The assessment conditions of subjective handle evaluation are critically important. Different skin hydrations of individuals affect notably the feel of a textile. A higher moisture level on the skin makes it more sensitive to the sense of touch (Mäkinen et al., 2005).

The evaluation is carried out in three different conditions: sight only, touch only and sight and touch together. During the assessment, in order to prevent the effect of colour and appearance on the assessments, wooden boxes with holes on the facing sides, through which the hands can easily go, can be used. Fabric samples are placed in these boxes prior to assessments. This helps the jury to assess the fabric without seeing it (Sülar & Okur, 2008b).

The first attempts of ranking and scaling the assessment methods in hand evaluation of textiles in an organized and quantitative manner were published as early as 1926 and have continued up to the present time and two basic procedures of subjective hand evaluation is proposed as follows: (Bakar, 2004; as cited in Howorth, 1964):

- a. Direct method - is based on principle of sorting of individual textiles to defined subjective grade in ordinal scale (e.g., 0 - very poor, 1 - sufficient, 5 - very good, 6 - excellent).
- b. Comparative method - is based on sorting of textiles according to subjective criterion of evaluation (e.g., ordering from textiles with the most pleasant hand to textiles with the worst hand) (Bakar, 2004). If the number of samples is high, the second approach can be considered rather time consuming (Sülar & Okur, 2007).

It is preferable to use a paired comparison technique during assessment, the so-called bipolar pairs of sensory attributes, such as “thin/thick” or “soft/harsh” (Mahar et al., 1990; as cited in Brand, 1964). For the same reason, fabric hand attributes are measured on specific scales thus avoiding the intrinsic weakness of descriptive terminology. In case of using bipolar descriptors in the assessment of the handle, control fabrics are better to be used for the training of the panel members. Control fabrics are chosen according to the related objective properties. The test results for objective properties that are related to sensory attributes were sorted in ascending order for each parameter. The fabrics with minimum, maximum and medium values are determined and used for the initial tests for the selection of the control fabrics (Sülar & Okur, 2007).

It is crucially important to convert the subjective assessment results to the numerical values for finding a relationship between objective measurements to analyze statistical evaluation. Therefore, using these types of ranking scale is preferable (Table 3).

1	...	5	...	10
thinnest	...	medium	...	thickest
1	...	5	...	10
softest	...	medium	...	stiffest
1	...	5	...	10
smoothest	...	medium	...	roughest
1	...	5	...	10
proper	...	medium	...	most proper

Table 3. Handle components and the rating scale (Sülar & Okur, 2008a)

This subjective hand evaluation system requires years of experience and can obviously be influenced by the personal preferences of the assessor as mentioned before. A fabric may be felt light, soft, mellow, smooth, crisp, heavy, harsh, rough, furry, fuzzy or downy soft. So there is a need to replace the subjective assessment of fabrics by experts with an objective machine-based system which will give consistent and reproducible results (Hu, 2008).

## 4.2 Objective evaluation of fabric handle

For a long time, handle has been estimated by the organoleptic method. The producers and users of textile products try to formulate in words the impression of touching the flat textile product. In general, fabric hand is primarily assessed subjectively in a few minutes. Although this is a fast and convenient sort of quality control, the subjective nature of fabric handle leads to serious variations in quality assessment (Sülar & Okur, 2008a) and does not analyze the core of the problem connected with the influence of factors creating the particular sensations. This was why in the 1930s investigations were commenced into an objective measurement of the features which are decisive for handle. The common goal in objective measurement systems was to eliminate the human element in hand assessment and develop quantitative factors that could be measured in a laboratory (Kocik et al., 2005).

Peirce was a forerunner of such investigations with his works connected with determining the bending rigidity and compressibility of flat textile products (Kocik et al., 2005; as cited in Pierce, 1930). At the turn of the 1960s, researchers from the Swedish Textile Institute (TEFO) (Kocik et al., 2005; as cited in Eeg-Olofsson, 1957; as cited in Eeg-Olofsson, 1959; as cited in Olofsson, 1965; as cited in Olofsson & Ogucki; 1966; as cited in Lindberg et al., 1961; as cited in Lindberg et al., 1960) carried out intensive investigations into this matter. These research works led to determining the dependencies between the features of flat textile products subjected to bending, buckling, shearing, and compressing, and the susceptibility of these products to manufacturing clothing. Lindberg (Kocik et al., 2005; as cited in Lindberg et al., 1960) was the first researcher who applied the theory of buckling for estimating the behaviour of fabrics in the clothing manufacturing process. Kawabata and Niwa were followers of Peirce and the Swedish researchers, who since 1968 have conducted research into handle. These investigations have been crowned by the design and construction of a measuring system which serves for objective estimation of handle (Kocik et al., 2005; as cited in Kawabata et al., 1973; as cited in Kawabata et al., 1996).

Objective assessment attempts to find the relationships between fabric hand and some physical or mechanical properties of a fabric objectively. It quantitatively describes fabric hand by using translation result from some measured values of relevant attributes of a fabric. Techniques used for objective hand evaluations are based on special instruments for measuring handle related properties (Bakar, 2004).

Several attempts have been made to measure fabric handle properties objectively described simply as "Fabric Objective Measurement (FOM)", and also a number of items of equipment have been introduced for this purpose (Hasani & Planck, 2009; Bishop, 1996).

### 4.2.1 Objective measurement systems

The KES-F system (Kawabata's Hand Evaluation System for Fabrics) was developed in Japan by the Hand Evaluation and Standardization Committee (HESC, established in 1972)

organized by Professor Kawabata. In this fabric objective measurement method, scientific principles are applied to the instrumental measurement and fabric low stress mechanical and surface properties such as fabric extension, shear, bending, compression, surface friction and roughness are measured. The fabric handle is calculated from measurements of these properties. Empirical equations for calculating primary hand values and total hand values were put forward by Kawabata and Niwa (Mäkinen et al., 2005; as cited in Kawabata, 1980; as cited in Shishoo, 2000).

The process of the subjective evaluation according to Kawabata can be given as follows (Bona, 1994):

Touch of fabric by hand	Detection of fabric basic mechanical properties such as bending, stiffness, etc.	Summarized expressions → about fabric characters by “primary hand”	Overall → judgement of fabric quality
Physiological sensing data processing in man’s brain			

The first part of Kawabata’s work was to find the important aspects of handle and the contribution of each to the overall rating of the fabric. For each category such as stiffness, smoothness, etc. were identified and the title of primary hand values were give. The original Japanese terms of these primary hand definitions together with English meanings are given in Table 4. The primary hand values are combined to give an overall rating for the fabric categories such as man’s summer suiting, man’s winter suiting, lady’s thin dress, and man’s dress short and knitted fabrics for undershirts. The conversion of the primary hand values is done by using a translation equation for a particular fabric category determined empirically. This total hand value is rated on a five point scale, where five is the best rating (Kawabata, 1980).

The second stage of Kawabata’s work was to produce a set of instruments with which to measure the appropriate fabric properties and then to correlate these measurements with the subjective assessment of handle. The aim was that the system would then enable any operator to measure reproducibility the total hand value of a fabric (Saville, 1999).

The Kawabata Evaluation System for Fabric (KES-F) which has been widely used since the 1970’s consists of four specialized instruments: FB1 for tensile and shearing, FB2 for bending, FB3 for compression and FB4 for surface friction and variation. A total of 16 parameters are measured at low levels of force (Table 5). The measurements are intended to simulate the fabric deformations found in use (Hu, 2008; Chen et al., 2001).

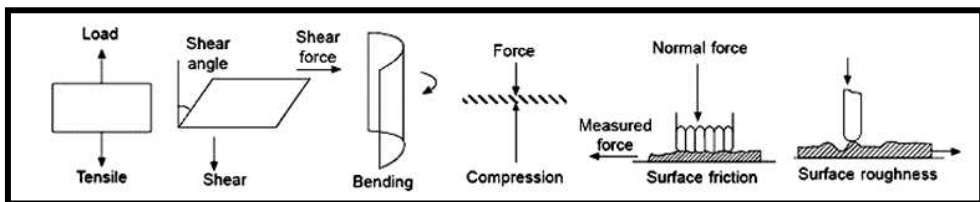


Fig. 7. Measuring principles of the KES system

Hand		Definition
Japanese	English	
<i>Koshi</i>	<b>Stiffness</b>	A stiff feeling from bending property. Springy property promotes this feeling. High-density fabrics made by springy and elastic yarn usually possess this feeling strongly.
<i>Numeri</i>	<b>Smoothness</b>	A mixed feeling come from smooth and soft feeling. The fabric woven from cashmere fiber gives this feeling strongly.
<i>Fukurami</i>	<b>Fullness and softness</b>	A bulky, rich and well-formed feeling. Springy property in compression and the thickness accompanied with warm feeling are closely related with this feeling ( <i>fukurami</i> means 'swelling').
<i>Shari</i>	<b>Crispness</b>	A feeling of a crisp and rough surface of fabric. This feeling is brought by hard and strongly twisted yarn. This gives a cool feeling. This word means crisp, dry and sharp sound made by rubbing the fabric surface with itself.
<i>Hari</i>	<b>Anti-drape stiffness</b>	Anti-drape stiffness, no matter whether the fabric is springy or not. (This word means 'spread').
<i>Kishimi</i>	<b>Scrooping feeling</b>	Scrooping feeling. A kind of silk fabric possesses this feeling strongly.
<i>Shinayakasa</i>	<b>Flexibility with soft feeling</b>	Soft, flexible and smooth feeling.
<i>Sofutosa</i>	<b>Soft touch</b>	Soft feeling. A mixed feeling of bulky, flexible and smooth feeling.

Table 4. The definitions of primary hand (Kawabata, 1980)

The characteristic values are calculated from recorded curves obtained from each tester both in warp and weft direction. Tensile properties (force-strain curve) and shear properties (force-angle curve) are measured by the same apparatus. Bending properties (torque-angle curve) are measured by bending first reverse sides against each other and after that the face sides against each other. Pressure-thickness curves are obtained by compression tester. The measurements of surface friction (friction coefficient variation curve) and surface roughness (thickness variation curve) are made with the same apparatus using different detectors.

The tensile properties are measured by plotting the force extension curve between zero and a maximum force of 500 gf/cm, the recovery curve as the sample is allowed to return to its original length is also plotted to give the pair of curves shown in Figure 8a. From these curves the following values are calculated (Saville, 1999):

Tensile energy  $WT$  = the area under the load strain curve (load increasing)

Linearity  $LT=WT/\text{area triangle } OAB$

Resilience  $RT=\text{area under load decreasing curve} / WT \times 100$

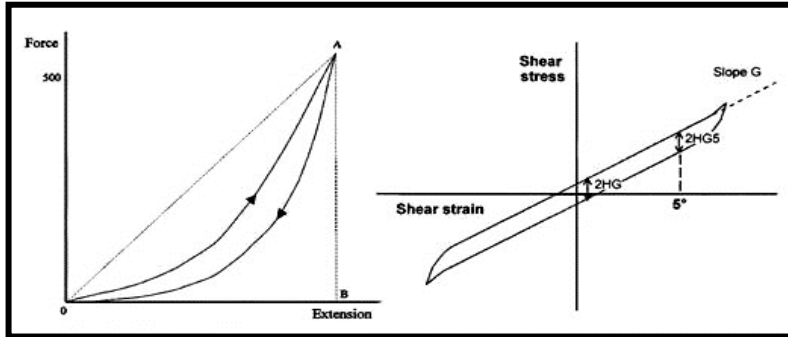


Fig. 8. (a) Load extension recovery curve (b) Hysteresis curve for shear (Saville, 1999)

Characteristic values measured in KES-F system			
KES- FB1	Tensile	LT	Linearity of load-extension curve
		WT	Tensile energy
		RT	Tensile resilience
	Shearing	G	Shear rigidity
		2HG 2HG5	Hysteresis of shear force at 0.5° shear angle Hysteresis of shear force at 5° shear angle
KES- FB2	Bending	B	Bending rigidity
		2HB	Hysteresis of bending moment
KES- FB3	Compression	LC	Linearity of pressure-thickness curve
		WC	Compressional energy
		RC	Compressional resilience
KES- FB4	Surface	MIU	Coefficient of friction
		MMD	Mean deviation of MIU, frictional roughness
		SMD	Geometrical roughness
Fabric construction	Weight	W	Weight per unit area
	Thickness	T	Thickness at 0.5 gf/cm <sup>2</sup>

Table 5. Characteristic values in KES-F system (Mäkinen et al., 2005; as cited in Kawabata, 1980)

In order to measure the shear properties, a sample in dimensions of 5cm x 20cm is sheared parallel to its long axis keeping a constant tension of 10 gf/cm on the clamp. The following quantities are then measured from the curve as shown in Figure 8b.

Shear stiffness  $G$  = slope of shear force-shear strain curve

Force hysteresis at shear angle of 0.5°  $2HG$  = hysteresis width of curve at 0.5°

Force hysteresis at shear angle of 5°  $2HG5$  = hysteresis width of curve at 5°

In order to measure the bending properties of the fabric, the sample is bent between the curvatures  $-2.5$  and  $2.5 \text{ cm}^{-1}$ , the radius of the bend is the reciprocal of the curvature as shown in Figure 9a. The bending moment required to give this curvature is continuously monitored to give the curve as shown in Figure 9b (Saville, 1999).

Compressibility is one of the most important properties in terms of fabric handle for the fabrics used in garment manufacture (Mukhopadyhay et al., 2002). The compression test for fabric is used to determine the fabric thickness at selected loads, and reflects the 'fullness' of a fabric (Hu, 2008).

The compression energy, compressibility, resilience and thickness of a specimen can be obtained by placing the sample between two plates and increasing the pressure while

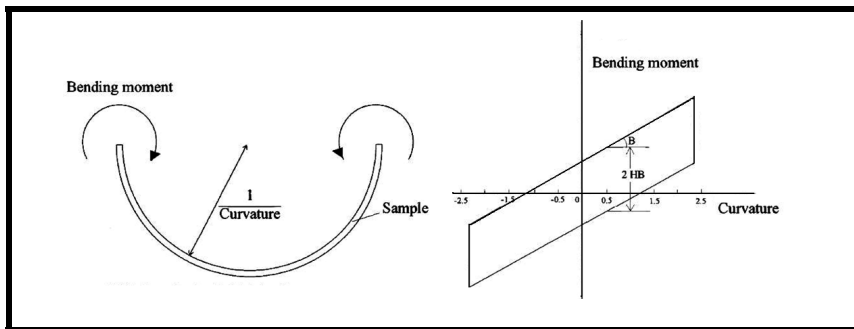


Fig. 9. a) Forces involving in fabric bending; b) Plot of bending moment against curvature (Saville, 1999)

continuously monitoring the sample thickness up to a maximum pressure of  $50 \text{ gf/cm}^2$ . A circular compressing board of  $2 \text{ cm}^2$  attached with a sensor is used to apply the force on the fabric specimen (Figure 10) (Saville, 1999).

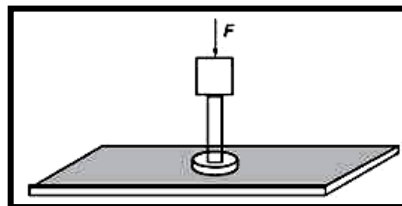


Fig. 10. Compression test on the KES-F system (Hu, 2008)

The surface friction is measured in a similar way by using a contactor which consists of ten pieces of the same wire as used in the surface roughness. A contact force of  $50 \text{ gf}$  is used in this case and the force required to pull the fabric past the contactor is measured. For the surface roughness, the contact force that the wire makes with the surface is  $10 \text{ gf}$  (Chen et al., 2001).

Kawabata developed through extensive human subjective evaluations of a range of fabric types and the ranking of characteristics. The weighing factors are believed to be appropriate



for the population within which the data were taken but there is some question as to the application of the same weighing factors in a different culture (Adanur, 2001). Critics still exist due to the high cost of the instrument. The system also requires experts for the interpretation of the resulting data. These deficiencies led to the development of another testing device called the FAST (Hu, 2004).

The Australian CSIRO designed and developed the FAST (Fabric Assurance by Simple Testing) set of instruments, as a simpler alternative to a KES system, which in terms of practicality and testing speed, go a long way towards meeting the requirements of garment makers, finishers and is designed to be relatively inexpensive, reliable, accurate, robust and simple to operate. Unlike the KES-F system, FAST only measures the resistance of fabric to deformation and not the recovery of fabric from deformation (Shishoo, 1995; Behery, 2005; Mazzuchetti et al., 2008; Potluri et al., 1995).

FAST gives similar information on the aesthetic characteristics of fabric as KES-F does, but in a simple manner, and is more suited to a mill environment. The FAST system includes FAST-1 for thickness, FAST-2 for bending, FAST-3 for extensibility and FAST-4 for dimensional stability. Through the objective measurements of fabric and a data set on a chart or 'fingerprint', manufacturers can identify fabric faults, predict the consequences of those faults and identify re-finishing routes or changes in production (Hu, 2008).

Characteristics measured in FAST system		Symbol	Unit	Device
Fabric weight		W	g/m <sup>2</sup>	
Compression	Total thickness	ST	mm	FAST-1
	Surface thickness		mm	
Bending	Bending length	B		FAST-2
Tensile	Warp elongation	E	%	FAST-3
	Weft elongation		%	
	Crosswise elongation		%	
Dimensional stability	Relaxation shrinkage	RS	%	FAST-4
	Hygral expansion	HE	%	

Table 6. List of fabric properties measured using FAST (Saville, 1999)

FAST-1 is a compression meter enabling the measurement of fabric thickness and surface thickness at two predetermined loads (Hu, 2004). The fabric thickness is measured on a 10 cm<sup>2</sup> area at two different pressures, firstly at 2 gf/cm<sup>2</sup> and then at 100 gf/cm<sup>2</sup>. This gives a measure of the thickness of the surface layer which is defined as the difference between these two values (Figure 11a). The fabric is considered to consist of an incompressible core and a compressible surface (Saville, 1999).

FAST-2 is a bending meter, which measures the bending length of the fabric. From this measurement, the bending rigidity of the fabric can be calculated. The instrument uses the cantilever bending principle described in BS: 3356. However, in FAST-2 the edge of the fabric is detected using a photocell. The bending rigidity, which is related to the perceived stiffness, is calculated from the bending length and mass/unit area. (Saville, 1999; Hu, 2004).

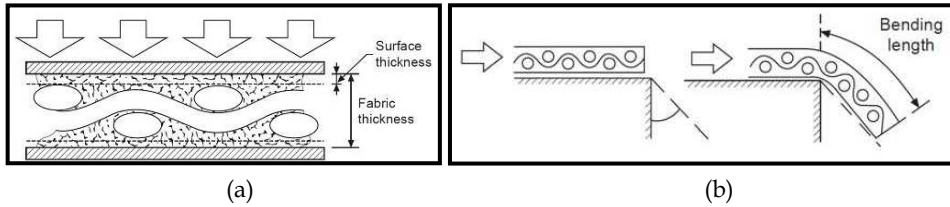


Fig. 11. (a) Measuring principle of the FAST-1 compression meter; (b) Measuring principle of the FAST-2 bending meter (Hu, 2004)

FAST-3 is an extension meter which operates on a simpler principle as shown in Figure 12a (Hu, 2004). The extension of the fabric is measured in the warp and weft directions at three fixed forces of 5, 20 and 100 gf/cm (sample size tested 100mm x 50mm). The extension is also measured on the bias in both directions but only at a force of 5gf/cm, this enables the shear rigidity to be calculated (Saville, 1999).

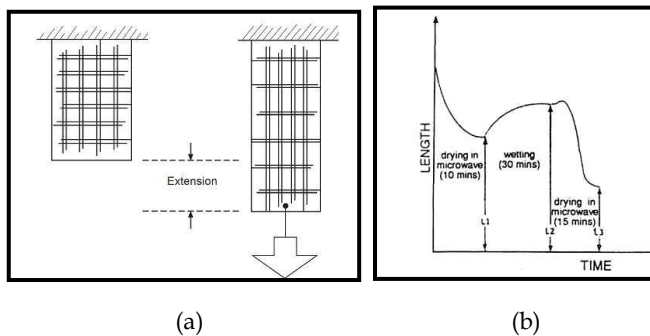


Fig. 12. (a) Measuring principle of the FAST-3 extension meter (Hu, 2004); (b) Dimensional stability curve (Bona, 1994)

The final component of FAST is a test method which measures the changes in the dimensions of fabrics that occur when the fabric is exposed to changing environmental conditions (Hu, 2004). A small amount of shrinkage (usually below 1%) is required for fabrics intended to be pleated. In order to measure dimensional stability the fabric is dried in an oven at 105°C and measured in both warp and weft directions to give the length  $L_1$ . It is then soaked in water and measured wet to give the wet relaxed length  $L_2$ . It is then re-dried in the oven and measured again to give the length  $L_3$ . The following values for dimensional stability are then calculated from these measurements for both warp and weft.

$$\text{Relaxation shrinkage} = \frac{L_1 - L_3}{L_1} \times 100(\%) \quad \text{Hygral expansion} = \frac{L_2 - L_3}{L_3} \times 100(\%)$$

Since the sensation is related to physical properties of the material, physical measurements constitute significant data in terms of objective evaluation. Disadvantages of the complex measuring systems such as high costs, difficulties in maintenance and reparation have resulted in conducting studies on improving simpler and individual instruments for each handle related objective fabric properties (Ozcelik et al., 2008).

**4.2.2 Individual objective measurement testers**

Shirley stiffness tester and circular bending rigidity tester for bending properties, cusick drape meter and sharp corner drape meter for drape properties, universal tensile testers for tensile and shear properties, thickness gauges for thickness and compression properties, universal surface tester and Frictorq for friction properties can be listed as commonly used simpler devices for measuring handle related properties of textile materials. Fabric extraction method and devices such as Griff-Tester (Kim & Slaten, 1999; Strazdienė & Gutauskas, 2005), robotic handling systems (Potluri et al., 1995) and various individual devices are some of the other objective measurement systems (Özçelik et al., 2008).

Cantilever stiffness tester supplies an easy way for measuring the fabric stiffness (Figure 13a). In the test, a horizontal strip of fabric is slid at a specified rate in a direction parallel to its long dimension, until its leading edge projects from the edge of a horizontal surface. The length of the overhang is measured when the tip of the specimen is depressed under its own mass to the point where the line joining the top to the edge of the platform makes a 41.5° angle with the horizontal. It is known as bending length (Figure 13b) and from this measured length, the flexural rigidity is calculated by using the formula given below (ASTM D 1388).

$G = 1.421 \times 10^{-5} \times W \times c^3$  ; where:  $G$  = flexural rigidity ( $\mu\text{joule/m}$ ),  $W$  = fabric mass per unit area ( $\text{g/cm}^2$ ) and  $c$  = bending length (mm).

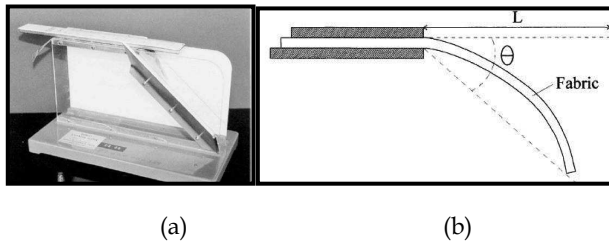


Fig. 13. (a) Cantilever stiffness tester, (b) Bending length (Saville, 1999)

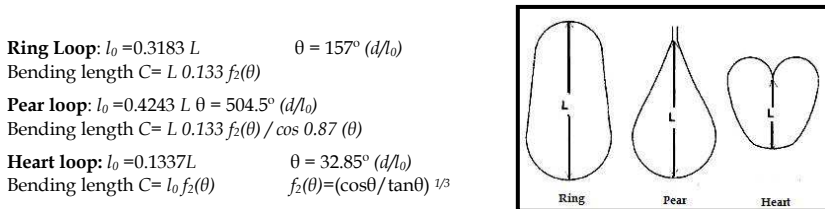


Fig. 14. Different shapes of hanging loops (Saville, 1999)

The cantilever method is not suitable for the fabrics that are too limp or show a marked tendency to curl or twist at a cut edge. The heart loop test can be used for these fabric types. A strip of fabric is formed into a heart-shaped loop. The length of the loop is measured when it is hanging vertically under its own mass (ASTM D 1388–08). The undistorted length of the loop  $l_0$ , from the grip to the lowest point is calculated (Saville, 1999; as cited in Peirce, 1930) for three different loop shapes: the ring, pear and heart shapes. If the actual length  $l$  of

the loop hanging under its own weight is measured, the stiffness can be calculated from the difference between the calculated and measured lengths  $d = l - l_0$ .

Another instrument which has the same working principle with Kawabata KES-F system is TH 7 bending rigidity tester. The instrument has clamp, which firstly rotates  $90^\circ$  to the front and after that comes to the starting point and moves  $60^\circ$  to the backwards. The required forces to bend the sample in different angles are recorded (Ozcelik & Mertova, 2005).

In circular bending rigidity test, that gives fabric stiffness in all direction, a plunger forces a flat, folded swatch of fabric through an orifice in a platform (Figure 15). The maximum force required to push the fabric through the orifice is an indication of the fabric stiffness (resistance to bending). The circular bend procedure gives a force value related to fabric stiffness (ASTM D 4032 - 08).

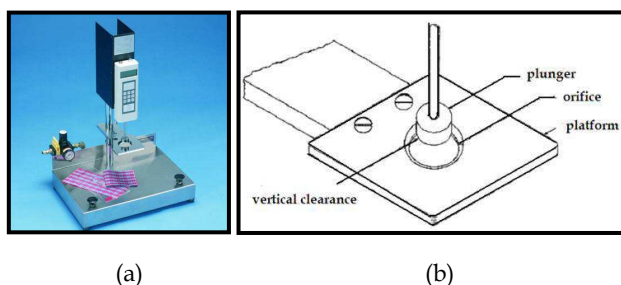


Fig. 15. (a) Circular bending rigidity tester ([www.sdlatlas.com](http://www.sdlatlas.com)), (b) Platform and plunger of the tester (ASTM D 4032 - 08)

Drape is the term used to describe the way a fabric hangs under its own weight (Saville, 1999). Basically, fabric drape is not an independent fabric property. It relates to fabric bending, shear, tensile, fabric thickness and fabric weight (Hu, 2004; as cited in Niwa & Seto, 1986; as cited in Collier, 1991; as cited in Hu & Chan, 1998).

In cusick drape meter, the specimen deforms with multi-directional curvature and consequently the results are dependent to a certain amount upon the shear and bending stiffness properties of the fabric. In the test, a circular specimen is held concentrically between two smaller horizontal discs and is allowed to drape into folds under own weight (Saville, 1999). A light is shone from underneath the specimen as shown in Figure 16a and a fabric drape profile can be captured in a two dimensional image by using a digital camera (Figure 16b). The drape profile can be observed from the computer screen and drape coefficient can be calculated by using image analysis software. The stiffer fabric means that the area of its shadow is larger compared to the unsupported area of the fabric so the higher the drape coefficient is. It is considered that the drape coefficient by itself is not sufficient for the drape characteristic of a fabric (Stylios & Powell, 2003; as cited in Stylios & Zhu, 1997) and therefore a feature vector, consisting of the average minima and average maxima fold lengths and the evenness of the folds is defined (Stylios & Powell, 2003; as cited in Ballard & Brown, 1982).

Measurement of drape angle by means of a special tool (table) is carried out by moving this sample towards the sharp corner of the table, in such way that the axis of the  $90^\circ$

angle coincides with the warp or weft direction. The fabric motion stops, when the peak of the corner reaches to the center of the sample. Then the fabric folds and forms a direct edge, whose inclination  $\varphi$  against the horizontal plane measured. The  $\sin \varphi$  value measured by means of simple ruler (Figure 16c), then characterizes the level of drape (Hes, 2009). The fabric becomes harder as the drape angle gets smaller (Ozcelik et al., 2008; Hes, 2004).

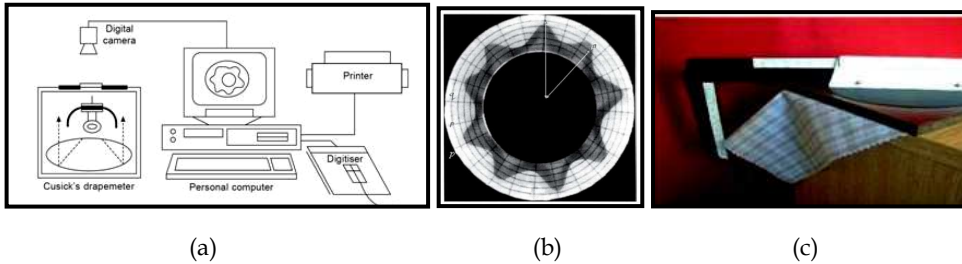


Fig. 16. The set up for the measurement of fabric drape profile: (a) Image analysis system, (b) Captured image on the drapemeter (Hu, 2004), (c) Sharp corner tester (Hes, 2004)

Friction coefficient is not an inherent characteristic of a material or surface, but results from the contact between two surfaces (Lima et al., 2005; as cited in Bueno et al., 1998). Two main ways are generally used to measure fabric friction. In one of these methods, as shown in Figure 17a, a block of mass ( $m$ ) is pulled over a flat rigid surface, which is covered with the fabric being tested. The line connected to the block is led around a frictionless pulley and connected to an appropriate load cell in a tensile testing machine. This can measure the force ( $F$ ) required both to start the block moving and also to keep it moving, thus providing static and dynamic coefficients of friction from the relation: Coefficient of friction  $\mu = F / (m.g)$  (Figure 17a).

The second method used for measuring fabric friction is the inclined plane as shown in Figure 17b. The apparatus is arranged so that the angle of the plane can be continuously adjusted until the block begins to slide. At this point, the frictional force ( $F$ ) is equal to component of the mass of the block parallel to the inclined plane (Saville, 1999).

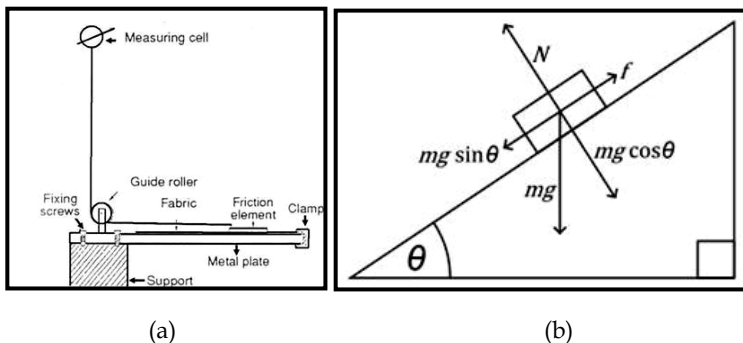


Fig. 17. Basic fabric friction measurement methods (Bona, 1994)

Frictorq is based on a new method to measure the coefficient of friction of the fabrics, using a rotary principle and, therefore, measuring torque. The upper body is a specially designed contact element, restricted to 3 small pads with an approximately square shape (covered by a number of calibrated steel needles), and placed over the fabric sample. This upper body is forced to rotate around a vertical axis at a constant angular velocity. Friction coefficient is again proportional to the torque measured with a precision torque sensor (Silva et al., 2010).

$$T = 3.F_a.r,$$

$$F_a = \mu.N,$$

$$N = P/3 \text{ and } \mu = T / (P.r)$$

where,  $r$  is the radius of the upper body,  $P$  is the vertical load and  $\mu$  is the coefficient of friction (Silva et al., 2010).

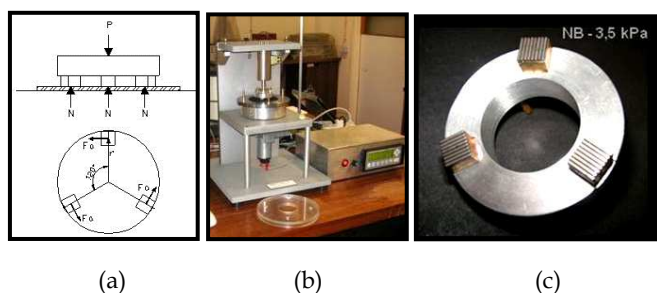


Fig. 18. (a) Loads in the measurement unit, (b) Frictorq instrument, (c) The upper body with 3 small pads (Silva et al., 2010)

Haptics, which derive from the Greek word *haptesthai*, means to touch and refers to simulate the feel of touch in the computer interface area (Govindaraj et al., 2003a). The other touch feedback systems do not have the sensitivity required for accurate simulation of fabric hand. PhilaU Haptic Device was developed to meet these requirements. During the development stage, the device called PHANToM<sup>®</sup> that uses a pen like probe to scan a virtual surface and generate the feel of surface, was used. By holding a pen with a stylus and moving the pen over a constructed surface in the virtual space, a feed back response was felt on the hand. The limitation of the device was that the contact with the virtual surface was over a line. However, it was possible to gain considerable information about a surface by moving a pencil-point across the surface, therefore it did not provide a tactile feeling (Govindaraj et al., 2003b, as cited in Katz, 1925). In order to overcome this limitation, the PhilaU Haptic Device (Figure 19) was designed as a combination force feed back and a tactile display. The device consists of a feeler pad at the end of an articulated arm joints, which is equipped with magnetic brakes, apply a force feed back to the hand holding the feeler pad assembly. The magnetic brakes get their input voltage proportional to surface friction of the fabric, while the tactile pins follow the contour. Together, the device provides a virtual fabric touch and feels (Govindaraj et al., 2003b).

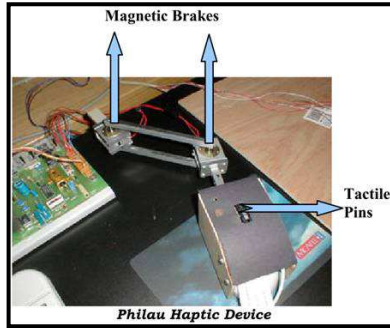


Fig. 19. Philau Haptic Device (Govindaraj et al, 2003a)

A robotic system developed by Potluri et al., designed for conducting all the fabric tests on a single sample, without operator intervention can be computed fabric properties such as tensile energy, shear stiffness, bending stiffness and compression energy. Uniform pressure is applied on the fabric sample by a manipulating device, attached magnetically to the robot arm, to avoid possible shear distortion or shear buckling (Potluri et al., 1995).

Several researches have been conducted for measuring the handle related mechanical properties of the fabrics by using universal tensile testers. The comprehensive handle evaluation system for fabrics and yarns (CHES-FY) is a kind of apparatus that is capable of measuring mass, bending, friction and tensile behavior just through one pulling-out test, and is able to characterize the handle of fabrics (Figure 20). The shape of a hung fabric was captured by a digital camera, and its weight was calculated. Then, a three-point bending in principle was utilized to model and analyze the bending properties of the fabric, and the corresponding formula was obtained for calculating the bending rigidity of the fabric (Du & Yu, 2007).

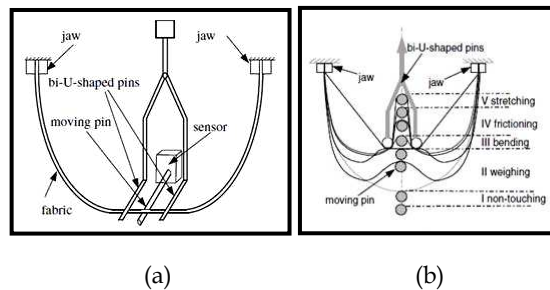


Fig. 20. (a) A schematic structure and (b) separated extraction steps of the CHES-FY (Du & Yu, 2007)

An alternative simple approach has been investigated by many researchers in order to predict fabric handle from the properties of fabric extraction through a ring or orifice (Wang et al., 2011; as cited in Alley & McHatton, 1978; Kim & Slaten, 1999). Extraction method is based on holding the sample at its centre and then pulling it through a ring of appropriate diameter by using a tensile tester (Yazdi & Shahbazi, 2006; as cited in Grover, 1993). For a

properly designed nozzle, if the fabric extraction process is carefully examined, it will be found that during the process the sample is deformed under a very complex low stress state including tensile, shearing and bending as well as frictional actions, similar to the stress state, when handling the fabric (Figure 21a) (Pan, 2006). The behaviour of the fabric during testing is recorded on the load-elongation chart of the tensile testing machine (Yazdi & Shahbazi, 2006). Consequently, all the information related to fabric hand is reflected by the resulting load-displacement extraction curve.

A universal test unit (KTU-Griff-Tester) (Figure 21b) is recently developed as textile hand evaluation method based on pulling a disc-shaped specimen through a rounded hole operating together with either the standard tensile testing machine or an individual drive (Strazdienė & Gutauskas, 2005; as cited in Grover et al., 1993). It allows registration of the specimen pulling force-deflection curve and capturing of the shape variation images of the specimen (Strazdienė & Gutauskas, 2005).

Previously conducted researchers have used only one feature of the curve, e.g. the peak or the slope at a point (Pan, 2007; as cited in Alley, 1976), and discarded the rest of the information (Pan, 2006; as cited in Pan & Yen, 1984, 1992). The PhabrOmeter™ Fabric Evaluation System based on the research by Pan and his co-workers (Pan, 2006; Pan et al., 1993) was introduced. When compared to the KESF and FAST systems, the PhabrOmeter system uses a single instrument capable of testing the low-stress mechanical and physical properties of the fabrics related to the fabric handle. The objective data, obtained from extraction curves are sagging of unloaded fabric across orifice, slope of incline, height of curve peak, position deflection at peak height, post-peak height, width of peak, slope of decline, deflection post-peak height, work area underneath the curve within the triangle obtained from the PhabrOmeter tester (Figure 22). By using these objective parameters, a series of multiple linear regression models are developed and successfully validated to predict eight handle characteristics considered important for the handle of next-to-skin fabrics such as overall handle and primary handle characteristics, such as rough-smooth, hard-soft, loose-tight, hairy-clean, warm-cool and greasy-dry (Wang et al., 2011).

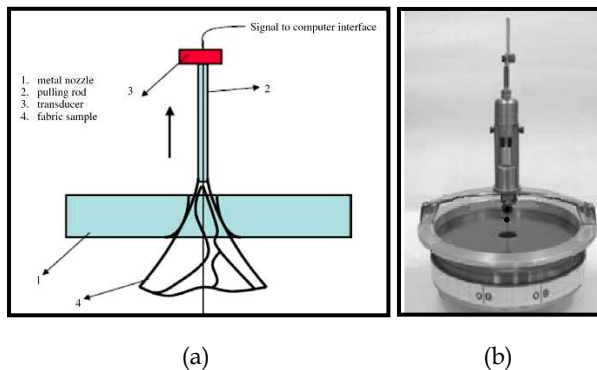


Fig. 21. (a) The fabric extraction technique (Pan, 2006) (b) KTU-Griff-Tester clamping device (Strazdienė & Gutauskas, 2005; as cited in Strazdiene et al., 2002)



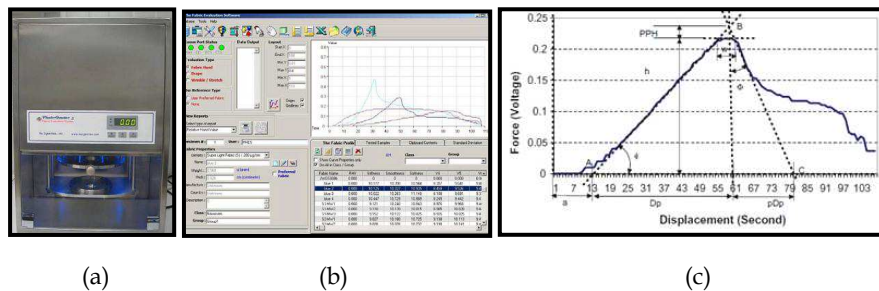


Fig. 22. (a) Hardware of PhabrOmeter model 3, (b) The user interface, (c) Extraction curve (Wang et al., 2011)

## 5. The relationship between the subjective evaluation and objective measurement of fabric handle

The subjective evaluation of fabrics leads to a set of linguistic terms strongly related to consumer preference but difficult to be quantized. It depends on many elements from raw materials to finishing processes. However, this evaluation restricts the scientific understanding of fabric performance for those who wish to design high-quality fabrics by engineering means. In the industry, the subjective evaluation is one of the main causes of conflict between producers and consumers on quality of products. Therefore, it is necessary to develop a normalized criterion representing the subjective evaluation or to replace it by an objective evaluation method. From any existing method of objective fabric evaluation, a set of precise quantitative data describing the fabric hand can be obtained but their relationship with the subjective evaluation is not completely discovered. Research has been done for modeling this relationship (Zeng & Koehl, 2003; as cited in Kawabata, 1996; as cited in Hu, 1993). However, progress in this field is rather slow because of the existence of uncertainties and imprecision in subjective linguistic expressions and the lack of mathematical models that constitute a nonlinear complex system for explaining the relationship between subjective and objective data, that, where no mathematical models are available (Zeng & Koehl, 2003).

Numerous methods such as Steven's law, rank correlation, linear regression model, multiple-factor analysis, weighted euclidean distance, component analysis, decision and information theory, canonical correlation methods and as intelligent techniques fuzzy logic-based methods, neural network statistical models and mathematical models have been introduced for the generation of a quantitative criterion characterizing the quality of textile products and modeling relationships between the subjective fabric hand evaluation and objective numerical data. Since all these methods require tedious computations and are thus inappropriate for providing quick responses to consumers, in recent works fuzzy comprehension evaluation, neural network aggregation of data, classification methods are widely used. Advantages of these techniques can be stated as computing with numerical data and words, computing with uncertainty and imprecision, taking into account nonlinear correlation, computing with few numbers of data (Bishop, 1996; Hui et al., 2004; Bakar, 2004).

The modeling and the simulation of textile fabrics represent an important field of scientific research. Several disciplines involve in this field, such as mathematics, mechanics, physics,

and informatics. This activity of research aims to produce simulations of textile fabrics behavior with more realism while remaining faithful to the physical and mechanical properties of this type of materials (Hedfi et al., 2011).

## 6. Conclusion

In this chapter, fabric sensorial comfort which has been studied by many researchers since the early 1900s, was dealt with in detail. As the studies are analyzed, it can be stated that, the previous studies generally focus on subjective evaluation whereas, in the last decades new objective evaluation methods and techniques simulating human tactile feeling and prediction methods are developed. It seems, as being an interesting research area, sensorial comfort will continue to attract the attention of researchers in the future.

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